IYPT 2018

6. Ring Oiler

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Problem Statement

"An oiled horizontal cylindrical shaft rotates around its axis at constant speed. Make a ring from a cardboard disc with the inner diameter roughly twice the diameter of the shaft and put the ring on the shaft. Depending on the tilt of the ring, it can travel along the shaft in either direction. Investigate the phenomenon."

Circular shaft with tracking dots



Ring resting on shaft with a tilt



Overview

Phenomenon

Reproduction of the Phenomenon & Experimental Measurements

Experimental Setup

Shaft-Motor setup, Camera setup, Tracker

Theoretical Model

Force balance, Torque balance and the two types of oscillations

Key Parameters

Tilts relative to the z- and y-axis, Reduction in the coefficient of friction, Shaft's angular velocity, Inner radius of ring

Conclusion

General Theory and Future Improvements in the Experiment

Phenomenon



Phenomenon Experimental Setup Theoretical Model Key Parameters Conclusion

Experimental Measure 1: Ring radii, thickness and depth

Depth:

• 3.36 ± 0.01 mm

Inner radii:

- Shaft: 14.62 ± 0.01 mm
- $17.54 \pm 0.01 \text{ mm}$
- $20.47 \pm 0.01 \text{ mm}$
- $23.39 \pm 0.01 \text{ mm}$
- $26.32 \pm 0.01 \text{ mm}$
- 27.78 ± 0.01 mm
- 29.24 ± 0.01 mm
- 30.70 ± 0.01 mm
- 32.16 ± 0.01 mm

Thicknesses:

- 4.76 ± 0.01 mm
- 14.76 ± 0.01 mm
- 24.69 ± 0.01 mm



Digital Vernier Caliper: $00.00-200.00\pm0.01~\text{mm}$



Conclusion

Phenomenon

Experimental Setup

Theoretical Model

Key Parameters

Experimental Setup

Phenomenon

Experimental Setup

Theoretical Model

Key Parameters



Experimental Setup



Phenomenon

Experimental Setup



Experimental Setup



Theoretical Model

Key Parameters

Experimental Measure 2: Shaft Wobble



Theoretical Model

Phenomenon

Experimental Setup

Theoretical Model

Key Parameters





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Geometry



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Theoretical Model Assumptions

- Ring is a rigid body
- Shaft spins along only the x-axis (i.e. ring is always in contact with the shaft)
- Air resistance is negligible
 - Verification:

•
$$F_{drag} = \frac{C_d \rho A v^2}{2}$$

•
$$C_d = 0.47, \, \rho = 1.225 \frac{kg}{m^{3'}} \, A \approx 0.04 m^2, \, A \approx 0.5 \, m^2$$

- $F_{drag} \approx 0.001 0.005$
- Thin layer of oil

Phenomenon

Experimental Setup

Theoretical Model

Key Parameters

Theoretical Model



Phenomenon Experimental Setup Theoretical Model Key Parameters Conclusion

Relative velocity



$$\overrightarrow{v_{rt}} = \overrightarrow{\omega_r} \times \overrightarrow{r_r}$$

$$\overrightarrow{v_{st}} = \overrightarrow{\omega_s} \times \overrightarrow{r_s}$$

$$\overrightarrow{v_{rel}} = \overrightarrow{v_{rt}} - \overrightarrow{v_{st}}$$
Since $\overrightarrow{F_f} \mid \mid - \overrightarrow{v_{rel}}$, the ring speeds up

until:

$$\overrightarrow{v_{rt}} = \overrightarrow{v_{st}}$$

$$\overrightarrow{\omega_r} \times \overrightarrow{r_r} = \overrightarrow{\omega_s} \times \overrightarrow{r_s}$$

$$\overrightarrow{v_{rt}} = \text{ring tangential velocity}$$

$$\overrightarrow{v_{st}} = \text{shaft tangential velocity}$$

Phenomenon Experimental Setup Theoretical Model Key Parameters Conclusion

Force balance



Experimental Setup

Phenomenon

 $F_g = m_r g$ $F_N = m_r g \cos \theta$ $F_f = \mu m_r g \cos \theta$

Initially:

Theoretical Model

$$\theta = 0, \omega_r = 0$$

After ring is placed on shaft:

$$\sum F_{y} = F_{N} \cos \theta - F_{G} + F_{F} \sin \theta = ma_{y}$$
$$\sum F_{z} = F_{F} \cos \theta - F_{N} \sin \theta = ma_{z}$$

Key Parameters

Force balance



$$\sum F_{y} = F_{N} \cos \theta - F_{G} + F_{F} \sin \theta = ma_{y}$$
$$a_{y} = g \sin \theta (\mu \cos \theta - \sin \theta)$$
$$\sum F_{z} = F_{f} \cos \theta - F_{N} \sin \theta = ma_{z}$$
$$a_{z} = g \cos \theta (\mu \cos \theta - \sin \theta)$$
When $a_{z}, a_{y} = 0$:
$$\mu_{k} = \tan \theta$$

Phenomenon Experimental Setup Theoretical Model Key Parameters Conclusion

Measured Value – Coefficient of Friction

Trial #	$ heta \pm 0.1^\circ$
1	5.9
2	5.7
3	6.1
4	6.3
5	6.2
6	6.0
7	6.1
8	6.3
9	6.1

$$\theta = 6.1 \pm 0.2^{\circ}$$

 $\mu = \tan \theta$

$$\mu_k = 0.11 \pm 0.01$$

(cardboard on aluminum with WD-40)

Experimental Setup

Theoretical Model

Key Parameters

Theoretical Model



Temporary Assumption



Relative Velocity



$$\overrightarrow{v_{rel}} = \overrightarrow{v_{rt}} - \overrightarrow{v_{st}}$$
$$\overrightarrow{F_f} \mid\mid - \overrightarrow{v_{rel}}$$

Phenomenon Experimental Setup Theoretical Model Key Parameters Conclusion

Force balance



$$\sum F_y = F_N - F_G = 0 = m_r a_y$$
$$a_y = 0$$
$$\sum F_z = F_f \sin \alpha = m_r a_z$$
$$a_z = \mu g \sin \frac{\alpha}{2}$$

$$\sum F_x = F_f \cos \theta = m_r a_x$$
$$a_x = \mu g \cos \frac{\alpha}{2}$$

Phenomenon Experimental Setup Theoretical Model Key Parameters Conclusion

Changing relative velocity



Center of mass now has an

acceleration in the x direction:



As v_{rx} increases, the x-component of F_f decreases, and a_x decreases:

Therefore, v_{rx} has a maximum velocity.

Phenomenon Experimental Setup Theoretical Model

Key Parameters

Theoretical Model



Phenomenon Experimental Setup Theoretical Model Key Parameters Conclusion

Types of Oscillations



- Driven completely by tilt in y-axis ($\beta > 0$)
- Driven completely by tilt in z-axis ($\alpha > 0$)

Transition from Type 1 to Type 2 during motion of ring



Phenomenon

Experimental Setup

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Key Parameters









Phenomenon

Experimental Setup

Theoretical Model

Key Parameters





Phenomenon Experimental Setup Theoretical Model Key Parameters Conclusion

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Transition – Type 1 \rightarrow Type 2

- Stage 1 (t = 0 to t = T/2)
 - *Period is restricted by period of type 1 oscillation (Amplitude is lower)*
- Stage 2 (t = T/2 to t = T)
 - Tilt in z-axis decreases
 - Lower restriction on period of motion (Higher amplitude)
- Stage 3 (t = T to t = infinity)
 - Motion of ring almost completely governed by type 2 oscillations

Transition – Type 1 \rightarrow Type 2

Transition between Type 1 and Type 2 Oscillations



Simulation - Basic Principle

In order to combine the previous basic principles, the *Explicit*

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Euler's Method was used:



Experimental Verification (x vs. t)



Experimental Data: X-Position vs. Time



Key Parameters

Phenomenon

Experimental Setup

Theoretical Model

Key Parameters

Why use oil?



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Why use oil?



Phenomenon

Experimental Setup

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Key Parameters

Different inner radii

Effect of Different Inner Radii of Ring on Period of Type 2 Oscillations



Different inner radii

Effect of Different Inner Radii of Ring on Amplitude of Type 2 Oscillations



Different shaft angular velocities

Effect of Different Angular Velocities on Period of Type 2 Oscillations



Different shaft angular velocities

Effect of Different Angular Velocities on Amplitude of Type 2 Oscillations



Different moment of inertias

Theoretical Effect of Different Moment of Inertia on Period of Type 2 Oscillations



Different moment of inertias

Theoretical Effect of Different Moment of Inertia on Amplitude of Type 2 Oscillations



Key Parameters



Conclusion

"An oiled horizontal cylindrical shaft rotates around its axis at constant speed. Make a ring from a cardboard disc with the inner diameter roughly twice the diameter of the shaft and put the ring on the shaft. Depending on the tilt of the ring, it can travel along the shaft in either direction. Investigate the phenomenon."



- Force balance, torque balance and change in angular momentum
- Effect of different tilts on the motion
- Amplitude and period of motion
- Coefficient of friction, inner radius, outer radius, and shaft angular velocity

Experimental Setup 7

Theoretical Model

Key Parameters

Thank you for listening



Appendix B

Movement of a masking tape roll with significant thickness along a shaft spinning at a constant angular velocity







Appendix C - Moment of inertia tensor

Due to three tilts in all three axis, the moment of inertia is defined as the following tensor:

$$I_{XX} \quad I_{XY} \quad I_{XZ} \quad I_{Xx} = \int (y^2 + z^2) dm \qquad I_{xy} = I_{yx} = -\int xy dm$$
$$I_{yX} \quad I_{yY} \quad I_{yZ} \quad I_{zX} \quad I_{zY} \quad I_{zZ} \quad I_{yy} = \int (x^2 + z^2) dm \qquad I_{yz} = I_{zy} = -\int yz dm$$

$$I_{zz} = \int (x^2 + y^2) dm$$
 $I_{xz} = I_{zx} = -\int xz \, dm$

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clear all % positive x is along shaft; % positive y is parallel and opposite to gravity; % positive z is out of the page

% approach: forces and then kinematics approach to linear dynamics % torque and change in angular momentum appraoach to rotational dynamics

% GIVEN CONSTANTS C_RING_MASS = 0.020; C_GRAVITY = -9.81; C_STEPS = 51; C_TOTAL_TIME = 1.67; C_ORIGIN = [0 0 0]; C_SHAFT_ANGULAR_VELOCITY = 150; C_FRICTION_COEFFICIENT = 0.1; C_INNER_RING_RADIUS = 2.54/100; C SHAFT RADIUS = 1.27/100;

% CALCULATED CONSTANTS
dt = C_TOTAL_TIME/(C_STEPS - 1);
% shaft angular velocity vector is strictly restricted to the x-direction
shaftAngularVelocity = [C_SHAFT_ANGULAR_VELOCITY 0 0];

% INITIAL VALUES

% first tilt is zero; second tilt is from above; leave third tilt as zero

- % reference frame: looking from positive y downwards; positive angle
- % is clockwise from negative z axis, negative angle is
- % counter-clockwise from negative z axis

I_TILT = [0 0.979 0];

Phenomenon

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% initial magnitude of ring angular velocity I RING ANGULAR VELOCITY = 75; % calculate components of ring angular velocity based on magnitude I RING ANGULAR VELOCITY = [I RING ANGULAR VELOCITY*cos(I TILT(2)) 0 I RING ANGULAR VELOCITY*sin(I TILT(2))]; % initial position vector I POSITION = $[0\ 0\ 0]$; % initial angle between the center of mass of the ring and the shaft when % looking straight down the shaft from the negative to the positive x % direction I COM ANGLE = 0.03; COMAngle = I COM ANGLE; % linear position | position = [0 -(C INNER RING RADIUS-(C SHAFT RADIUS/2))*cos(COMAngle) -(C INNER RING RADIUS-(C SHAFT RADIUS/2))*sin(COMAngle)]; l_position = l_position + l_POSITION; | velocity = [0 0 0];| acceleration1 = [000];r angularVelocity = I RING ANGULAR VELOCITY; l outerShaftVelocity = cross(shaftAngularVelocity, [0 cos(COMAngle)*C_SHAFT_RADIUS sin(COMAngle)*C_SHAFT_RADIUS]); % assign y as 1, find other components relative to 1, to get vector % direction u directionFromCOMToContactPoint = [-tan(COMAngle)*(r angularVelocity(1)/r angularVelocity(3)) 1 tan(COMAngle)]; % find vector with magnitude of inner ring radius, and direction of vector % calculated right before this one u COMToContactPoint = [(C INNER RING RADIUS/norm(u directionFromCOMToContactPoint))*u directionFromCOMToContactPoint(1) (C_INNER_RING_RADIUS/norm(u_directionFromCOMToContactPoint))*u_directionFromCOMToContactPoint(2) (C INNER RING RADIUS/norm(u directionFromCOMToContactPoint))*u directionFromCOMToContactPoint(3)]; l tangentialVelocity = cross(r angularVelocity, u COMToContactPoint) + l velocity; I_relativeLinearVelocity = I_outerShaftVelocity - I_tangentialVelocity;

Theoretical Model

% forces

f_gravity = [0 C_GRAVITY*C_RING_MASS 0]; f_normal = [0 -C_GRAVITY*C_RING_MASS -C_GRAVITY*C_RING_MASS*tan(COMAngle)]; f_friction = [((norm(f_normal)*C_FRICTION_COEFFICIENT)/norm(l_relativeLinearVelocity))*l_relativeLinearVelocity(1) ((norm(f_normal)*C_FRICTION_COEFFICIENT)/norm(l_relativeLinearVelocity))*l_relativeLinearVelocity(2) ((norm(f_normal)*C_FRICTION_COEFFICIENT)/norm(l_relativeLinearVelocity))*l_relativeLinearVelocity(3)]; f_net = f_gravity + f_normal + f_friction;

```
t_normal = cross(u_COMToContactPoint, f_normal);
t_friction = cross(u_COMToContactPoint, f_friction);
t net = t normal + t friction;
```

```
% center of mass

l_acceleration2 = l_acceleration1 + f_net/C_RING_MASS;

l_velocity = (0.5*(l_acceleration1 + l_acceleration2))*dt;

px(1) = l_position (1);

py(1) = l_position(2);

pz(1) = l_position(3);

l_position = l_position + (l_velocity * dt) + (0.5*(0.5*(l_acceleration1 + l_acceleration2))*dt*dt);
```

t = 0;

```
% angular momentum

r_MOI = 0.5;

r_angularMomentum = r_MOI * r_angularVelocity;

t_net_temp = [t_net(1) t_net(2) t_net(3)];

r_angularMomentum = r_angularMomentum + (t_net_temp*dt);

r_angularVelocity = r_angularMomentum / r_MOI;
```

rx(1) = 0;



```
\label{eq:steps-1} \begin{split} &\text{for } i = 1\text{:}C\_\text{STEPS}-1\\ & t(i\text{+}1) = t(i) + dt; \end{split}
```

f_gravity = [0 C_GRAVITY*C_RING_MASS 0]; f_normal = [0 -C_GRAVITY*C_RING_MASS -C_GRAVITY*C_RING_MASS*tan(COMAngle)]; f_friction = [((norm(f_normal)*C_FRICTION_COEFFICIENT)/norm(l_relativeLinearVelocity))*l_relativeLinearVelocity(1) ((norm(f_normal)*C_FRICTION_COEFFICIENT)/norm(l_relativeLinearVelocity))*l_relativeLinearVelocity(2) ((norm(f_normal)*C_FRICTION_COEFFICIENT)/norm(l_relativeLinearVelocity))*l_relativeLinearVelocity(3)]; f_net = f_gravity + f_normal + f_friction;

```
t_normal = cross(u_COMToContactPoint, f_normal);
t_friction = cross(u_COMToContactPoint, f_friction);
t net = t normal + t friction;
```

```
l_acceleration1 = l_acceleration2;
```

```
l_acceleration2 = l_acceleration1 + f_net/C_RING_MASS;
l_velocity = (0.5*(l_acceleration1 + l_acceleration2))*dt;
px(i+1) = l_position(1);
py(i+1) = l_position(2);
pz(i+1) = l_position(3);
l_position = l_position + (l_velocity * dt) + (0.5*(0.5*(l_acceleration1 + l_acceleration2))*dt*dt);
```

```
r_angularMomentum = r_angularMomentum + (t_net_temp*dt);
r_angularVelocity = r_angularMomentum / r_MOI;
```

```
rx(i+1) = r_angularVelocity(2);
```

COMAngle = atan(I_position(2)/I_position(3));

l_outerShaftVelocity = cross(shaftAngularVelocity, [0 cos(COMAngle)*C_SHAFT_RADIUS sin(COMAngle)*C_SHAFT_RADIUS]);

% assign y as 1, find other components relative to 1, to get vector

% direction

```
u_directionFromCOMToContactPoint = [-tan(COMAngle)*(r_angularVelocity(1)/r_angularVelocity(3)) 1 tan(COMAngle)];
```

% find vector with magnitude of inner ring radius, and direction of vector

% calculated right before this one

u_COMToContactPoint =

 $[(C_INNER_RING_RADIUS/norm(u_directionFromCOMToContactPoint))*u_directionFromCOMToContactPoint(1)$

(C_INNER_RING_RADIUS/norm(u_directionFromCOMToContactPoint))*u_directionFromCOMToContactPoint(2)

```
(C\_INNER\_RING\_RADIUS/norm(u\_directionFromCOMToContactPoint))*u\_directionFromCOMToContactPoint(3)];
```

```
L_tangentialVelocity = cross(r_angularVelocity, u_COMToContactPoint) + l_velocity;
```

```
l_relativeLinearVelocity = l_outerShaftVelocity - l_tangentialVelocity;
```

end

```
figure(1);
```

plot(t, px); hold on;

title('Effect of different angular velocities on x-position vs. Time');

xlabel('Time (s)');

ylabel('X-Position (m)');

legend('50 rad/s','100 rad/s','150 rad/s','Location','northwest')

Phenomenon Experimental Setup

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Key Parameters

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References

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Concluding Remarks

"An oiled horizontal cylindrical shaft rotates around its axis at constant speed. Make a ring from a cardboard disc with the inner diameter roughly twice the diameter of the shaft and put the ring on the shaft. Depending on the tilt of the ring, it can travel along the shaft in either direction. Investigate the phenomenon."

Response to the Opponent

- 1. Opponent's Point 1
- 2. Opponent's Point 2
- 3. Opponent's Point 3

Response to the Reviewer

- 1. Opponent's Point 1
- 2. Opponent's Point 2

Torque Balance



Experimental Setup

Phenomenon

With respect to the center of mass of the ring, only the friction force has a torque:

$$\overrightarrow{\tau_{net}} = \overrightarrow{\tau_f}$$
$$\overrightarrow{\tau_{net}} = \overrightarrow{r_r} \times \overrightarrow{F_f}$$

Initially:

Theoretical Model

 $\vec{L} = 0$

After ring is placed on shaft:

Key Parameters

$$\frac{d\vec{L}}{dt} = \overrightarrow{\tau_{net}}$$